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"Review – Microstructure Control and Function Expression Using Metal 3D Additive Manufacturing in the Digital Age"

Takayoshi Nakano, Takuya Ishimoto, Ryosuke Ozasa and Aira Matsugaki

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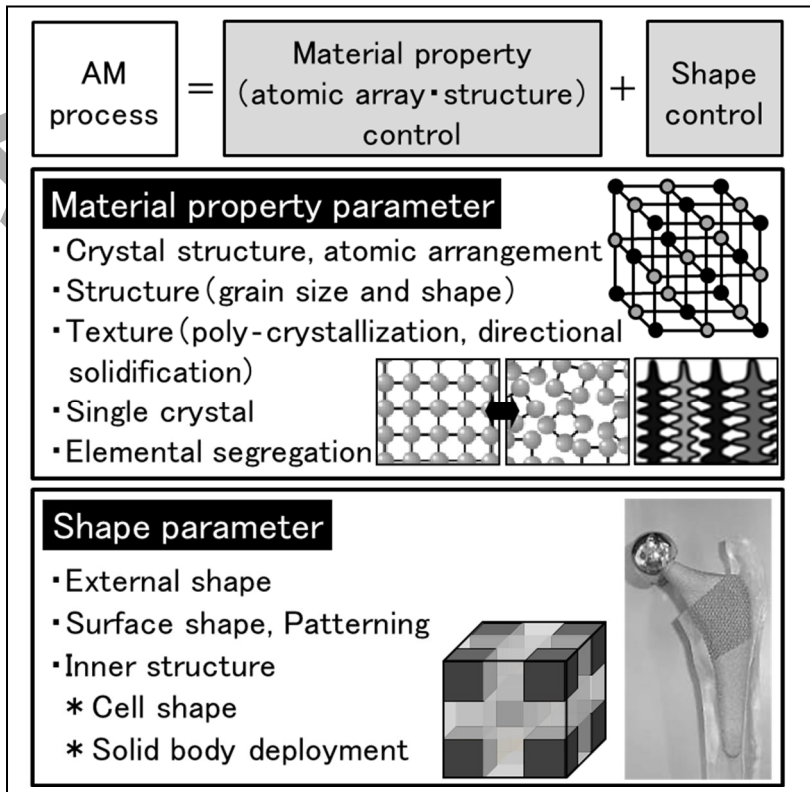
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Advance View

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# Graphical Abstract

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1 Review – Microstructure Control and  
2 Function Expression Using Metal 3D  
3 Additive Manufacturing in the Digital  
4 Age\*<sup>1</sup>

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6 Takayoshi Nakano<sup>1,2,\*2</sup>, Takuya Ishimoto<sup>1,2</sup>, Ryosuke  
7 Ozasa<sup>1,2</sup>, and Aira Matsugaki<sup>1,2</sup>

8

9 1 Division of Materials and Manufacturing Science, Graduate School of  
10 Engineering, Osaka University, 2-1 Yamada-Oka, Suita, Osaka 565-0871,  
11 Japan

12 2 Anisotropic Design and Additive Manufacturing Research Center,  
13 Osaka University, 2-1 Yamada-Oka, Suita, Osaka 565-0871, Japan

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19 \*<sup>2</sup> Corresponding author: Takayoshi Nakano; E-mail:  
20 nakano@mat.eng.osaka-u.ac.jp

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1    **Abstract**

2    3D Additive Manufacturing is the heaven-sent child for Internet  
3    of Things (IoT) in the digital age, and is a process that can be  
4    used for customized design and production. In particular, metal  
5    Additive Manufacturing enables not only the fabrication of  
6    complex shapes but also the control of crystal orientation at the  
7    atomic level by locally melting and solidifying the metal material,  
8    thereby realizing high functionality of the product through  
9    simultaneous design of shape and materials properties. Therefore,  
10   it is expected to be applied in various social infrastructure fields  
11   including medical, energy-related, aerospace, and automotive,  
12   and also as a means of adding high value. In this review article,  
13   the new manufacturing concept that can be realized by metal  
14   additive manufacturing is introduced.

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17    *Keywords: powder bed fusion, crystallographic texture,*  
18    *anisotropy, materials integration (MI) system, cross-*  
19    *ministerial strategic innovation promotion (SIP)*  
20    *program*

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## 1 **1. Introduction**

2 The power of monozukuri that drives the manufacturing  
3 industry in Japan continues to significantly influence the global  
4 economy. Low-variety/mass-production processes have become a  
5 commodity; however, manufacturing systems are transforming to  
6 achieve mass customization in the form of high-variety/low-  
7 volume production and high-variety/mass-production. This  
8 accelerated development of high-value-added products has  
9 significantly changed the global manufacturing landscape<sup>1-4</sup>). As  
10 the 4th Industrial Revolution approaches, represented by  
11 “Society 5.0” in Japan, and as digitalization grows in the form  
12 of the Internet of Things (IoT), artificial intelligence (AI), big-  
13 data construction/analysis, digital transformation (DX), cyber-  
14 physical systems (CPS), and materials integration (MI) systems,  
15 great expectations have been placed on three dimensional (3D)  
16 additive manufacturing (AM), which can be considered the  
17 offspring of the IoT. Furthermore, computer simulations (forward  
18 problem/inverse design analysis), 3D/4D design, material  
19 development, material manufacturing processes, surface  
20 treatment technologies, processing/joining technologies, and  
21 quality control systems are being constructed as whole systems  
22 to serve as new manufacturing platforms that support the key  
23 technologies of AM that correspond to digitalization.

24 In this review paper, we focus on the metal AM, which will  
25 support manufacturing in the future, and introduces the Osaka

1 University Anisotropic Design & Additive Manufacturing  
2 Research Center affiliated with graduate school of engineering,  
3 Osaka university (referred to as Osaka University AM Center).  
4 Furthermore, we present social trends in the field, such as  
5 national projects related to metal AM, functional design by  
6 complex shape designs and by microstructure control at the  
7 atomic level enabled via metal AM accompanied by DX.

## 9 **2. Osaka University Metal AM Center**

10 In December 2014, the Osaka University AM Center was  
11 established (Fig. 1), equipped with powder bed fusion (PBF)  
12 metal AM equipment that uses electron or laser beams as heat  
13 sources, and various tools that enable shape design and quality  
14 control, including in-process monitoring<sup>1)</sup>. The center also  
15 implements computational simulations to predict the temperature  
16 and stress fields, material structure, and atomic arrangement of  
17 the manufactured material via the metal AM process, while also  
18 developing tools that enable these processes. Recently, research  
19 and development has been conducted on an MI system that  
20 utilizes inverse design analysis, which enables the search for the  
21 optimum modeling conditions for metal AM process parameters  
22 using machine learning as an AI method to optimize the shape  
23 and function of the required molded objects<sup>5)</sup>. Using MI systems  
24 leads to the effective utilization of metal AM and high added  
25 value of various functions, such as mechanical properties,

1 corrosion and oxidation resistance, surface functionalization,  
2 and biocompatibility of molded materials<sup>6-18</sup>). The Osaka  
3 University Metal AM Center has two electron beam (Arcam Q10  
4 and a domestic machine) and two laser beam (EOS M290) metal  
5 AM machines; the center conducts research and development and  
6 actively supports companies, research institutions, and other  
7 universities from its neutral standpoint as a university<sup>1</sup>).

8 Figure 2 shows a conceptual diagram of anisotropic materials  
9 science, which forms the basis of the design concept and theory  
10 of the Osaka University Metal AM Center. The design policy of  
11 the center is to improve material functionality using a  
12 hierarchical structure based on isotropy /anisotropy<sup>1</sup>). In contrast  
13 to many artificial materials, e.g., existing metallic materials,  
14 designed to exhibit isotropic functions, most natural materials  
15 have an anisotropic structure such that functionality is achieved  
16 in the required direction in 3D, i.e., they have anisotropic  
17 structures in multiscale<sup>19</sup>).

18 Figure 3 shows the anisotropic microstructure of living  
19 bones<sup>20,21</sup>). Bones are mainly constructed from a coherent  
20 relationship between type I collagen and apatite crystallites<sup>22</sup>);  
21 however, the *c*-axis orientation of the apatite crystallites along  
22 the collagen fibers changes, reflected in the *in vivo* stress  
23 distribution. Collagen and apatite crystallites exhibit a  
24 preferential *c*-axis alignment to the direction of the maximum  
25 principal stress vector, resulting in high strength in the

1 orientation direction. The crystallographic texture in living  
2 bones is a good example of high functionality in a required  
3 direction; healthy and normal anisotropy is typically lost in  
4 diseased or regenerated bones and some genetically mutated  
5 mice<sup>22-26</sup>). Furthermore, osteocalcin is an important protein that  
6 controls the crystallographic consistency of collagen and  
7 apatite<sup>27</sup>).

8 Anisotropic materials science can be defined as a “science  
9 related to the research and development of materials and  
10 elucidation of the mechanism for exhibiting the ultimate high-  
11 performance properties in the required direction.” Metal AM is  
12 the ultimate means of freely producing objects that include such  
13 anisotropy<sup>28,29</sup>). Therefore, metal AM is one of the most suitable  
14 processes for creating individually customized substitutes for  
15 living bones<sup>1,29</sup>).

### 17 **3. National Projects Related to Metal Additive Manufacturing** 18 **in Japan**

19 Metal AM has attracted significant research attention  
20 domestically and internationally, with various related large-scale  
21 projects promoted in Japan. For example, the Cross-Ministerial  
22 Strategic Innovation Promotion (SIP) Program 1st  
23 Phase/Innovative Design and Production Technology ((Program  
24 Director: Dr. Naoya Sasaki; Funding (Management) Agency:  
25 NEDO), which started in 2014, involves the research and



1 development of high value-added design using metal AM  
2 equipment and high functionality through microstructure control  
3 of metallic materials<sup>30</sup>). The Monozukuri Revolution Program  
4 centered on 3D modeling technology by the Ministry of Economy,  
5 Trade and Industry (Technical Development of Next Generation  
6 Type 3D Printer for Industry), which also started in 2014, began  
7 developing next-generation domestic industrial metal AM  
8 equipment. Furthermore, the Technology Research Association  
9 for Future AM (TRAFAM) (President: Professor Hideki Kyogoku,  
10 Kinki University) continues to promote the construction of  
11 world-class next-generation industrial 3D printers and ultra-  
12 precision 3D modeling systems<sup>31</sup>).

13 The Cross-Ministerial SIP 2nd Phase/Materials Integration for  
14 Revolutionary Design System of Structural Materials<sup>5</sup>) (Program  
15 Director: Dr. Yoshinao Mishima; Funding (Management) Agency:  
16 JST), which started in 2018, aims to utilize the technical base of  
17 MI systems developed in Japan to construct the first MI  
18 development system that supports inverse design MI, which  
19 designs materials and processes based on desired performance.  
20 Targeting powder and metal AM materials, the project aims to  
21 utilize existing materials databases and build a database that  
22 supports new processes and evaluation technologies. The project  
23 aims to realize an inverse design MI system that fuses materials  
24 and information engineering and yields a material revolution that  
25 reduces the development period and cost of social

1 implementation. Across three domains (A, B, and C), 13 teams  
2 from 44 institutions, including industry, academia, and  
3 government, were working together.

4 The three domains are as follows. Domain A, “Establishment  
5 of the inverse design MI basis for advanced structural materials  
6 and processing,” aims to establish an MI development system to  
7 realize Society 5.0, proposes the required structure and  
8 properties of materials to fulfill their desired performance, and  
9 enables the potential processing of such materials. Domain B,  
10 “Applications of the Inverse Design MI to Actual Structural  
11 Materials (Carbon fiber reinforced plastics: CFRP),” aims to  
12 develop technologies to improve the property and productivity of  
13 CFRP, which are becoming widely used as materials for  
14 lightweight structure, using MI development and lead the world  
15 in the development of transport equipment such as aircrafts.  
16 Domain C, “Applications of the inverse design MI to actual  
17 structural materials (3D powder processing),” aims to realize  
18 innovative materials and processes using MI development, with  
19 a focus on powders of heat-resistant alloys with intense  
20 development competition and ceramics which are super high  
21 temperature heat-resistant materials for next-generation  
22 transportation and energy equipment, to strengthen industrial  
23 competitiveness in Japan.

24 The A2 (“Processing design”), C1 (“Development of AM  
25 process for Ni-based alloys”), and C4 (“Development of powder

1 manufacturing process and basic technologies for high  
2 performance TiAl based alloy turbine blades”) teams are based at  
3 the Osaka University Metal AM Center and lead the work on the  
4 social implementation of the MI system with mutual organic  
5 collaboration. The Osaka University Metal AM Center oversees  
6 the A2 team’s research on MI system technologies to accelerate  
7 the development of Ni-based super alloys, Ti-based alloys, and  
8 super heat-resistant ceramics, which are of crucial importance  
9 for aerospace and energy research, while also developing  
10 modules and workflows necessary for predicting the  
11 performances of target materials and processing. By utilizing the  
12 inverse problem analyses, they aim to establish a method to  
13 suggest appropriate materials and optimal processing conditions  
14 for a given desired performance. The author (Takayoshi Nakano)  
15 is the leader of Domain C; the C1 team considers the AM process  
16 for Ni-based alloys, which is an advanced process that can lead  
17 to innovations in the shape of parts and materials properties and  
18 is expected to be applied to combustion burners for hydrogen gas  
19 turbines. However, AM requires complex and wide-range  
20 parameter optimization. In their research, the C1 team aims to  
21 improve the durability of combustion burners by fabricating new  
22 Ni-based alloys found by the MI system for AM. The C4 team  
23 aims to develop superior low-pressure turbine blades using  
24 powder processes of metal injection molding and AM and build a  
25 sophisticated MI system for inverse problems in collaboration

1 with other universities and industries. The MI system consists of  
2 a property prediction module microstructure design module, and  
3 process design module based on experiments and theoretical  
4 calculations and successfully allows the design of novel alloys  
5 to meet the required mechanical properties and geometries for  
6 both MIM and AM processes. The outcomes of this project will  
7 enhance industrial strength in Japan.

8 The C1 team applied laser beam-based metal AM to Ni-based  
9 alloys developed by the MI system; their method is an advanced  
10 process that could yield innovations in both the shape of parts  
11 and material properties and could be applied to combustion  
12 burners for power generation gas turbines that are exposed to  
13 high temperatures and have complicated flow paths. However,  
14 optimizing the complex and diverse parameters required by this  
15 laser metal AM process is difficult. The C1 team is searching for  
16 conditions in cyberspace using the MI system while also pursuing  
17 the optimization of conditions and demonstration of the unique  
18 functions of 3D AM components. In other words, they are working  
19 with the MI system for AM to verify the cyberspace process  
20 conditions in physical space and conduct demonstrations,  
21 including developing new Ni-based alloys; the Osaka University  
22 AM Center is building a basic database to build the MI  
23 infrastructure, optimizing the laser metal AM processes, and  
24 developing heat-resistant new alloys. The MI system will be  
25 integrated into the National Institute for Materials Science

1 (NIMS), and a consortium-type Japan-wide operation system is  
2 being constructed<sup>32</sup>).

#### 3 4 **4. Control of Shape and Material properties Using Metal** 5 **Additive Manufacturing**

6 AM is often considered for modeling 3D objects from simple  
7 to complex shapes. The main purpose of modeling metallic and  
8 ceramic materials using polymers and binders as raw materials is  
9 to control the shape of the material. Meanwhile, even with a  
10 molded object that has only undergone shape control, when a  
11 specific part is selectively melted/solidified by a heat source  
12 such as a laser or an electron-beam, temperature distribution  
13 effects, such as the migration velocity of the solid-liquid  
14 interface during solidification and the thermal gradient, induce  
15 cell growth with a preferred orientation and dendrite growth.  
16 Further, layer-by-layer modeling due to the influence of epitaxial  
17 growth and cyclic thermal profiles change the microstructure in  
18 a complex manner<sup>7,33</sup>). Hence, the PBF and directed energy  
19 deposition (DED) methods, which directly melt raw metal  
20 materials, control shape parameters as well as material properties,  
21 such as material structure and atomic arrangement. According to  
22 the often-used solidification map<sup>34</sup>), material properties, ranging  
23 from amorphous, polycrystal, columnar, and single crystal, can  
24 be controlled by controlling compositional supercooling and  
25 nucleation/growth conditions.

1 Figure 4 summarizes the material property (material structure  
2 and atomic arrangement) and shape parameters that can be  
3 controlled by metal AM. The material property parameters of  
4 metallic materials are directly linked to the mechanical  
5 properties and functionality of the modeled object; hence,  
6 methods for designing material properties become the deciding  
7 factor for the high added value of manufacturing using metal AM.  
8 Controlling functions while considering isotropy/anisotropy  
9 provides high functionality in a specified direction and can lead  
10 to the formation of specific material structures and expression of  
11 higher functions<sup>1,4,11</sup>.

12 Parameters involved in controlling the shape and material of a  
13 molded object are usually expressed in terms of energy density  
14 per unit volume ( $E$ ), where  $E$  is a function of power ( $P$ ), beam  
15 scanning speed ( $v$ ), scanning interval ( $w$ ), and layer thickness ( $h$ ),  
16 as in Eq. (1), where  $E$  has units of  $J/m^3$ .

$$17 \quad E = \frac{P}{v \cdot w \cdot h} \quad (1)$$

18  $E$  helps select process parameters for producing an optimal  
19 modeled object. However,  $E$  is essentially the amount of energy  
20 input to a unit volume; energy loss due to heat dissipation to the  
21 surroundings is not considered. The shape and material structure  
22 design of a modeled object requires controlling the heat  
23 distribution based on heat conduction and transfer; the shape of  
24 the molten pool formed by scanning the heat source and  
25 controlling the temperature distribution around the object,

1 including the thermal gradient, are particularly important.  
2 Therefore, optimizing the melting conditions using a thermal  
3 simulation that considers heat dissipation enables the  
4 identification of non-melted, optimally melted, and excessively  
5 melted conditions, and the optimization of the shape parameters.  
6 Additionally, material property parameters can be optimized by  
7 optimizing the shape of the molten pool and thermal gradient  
8 based on the temperature distribution and fully utilizing various  
9 computer simulation methods, such as phase field simulation<sup>35,36</sup>).

#### 11 **4.1. Control of shape parameters**

12 In metal AM, the shape of a structure is designed in 3D-CAD,  
13 where any three-dimensional shape can be controlled. Optimizing  
14 the outer and inner shapes makes it possible to express the  
15 desired functional characteristics, including isotropy/anisotropy.

16 Figure 5 shows Young's modulus of a modeled object, in which  
17 27 cubic elements ( $3 \times 3 \times 3$ ) are combined arbitrarily along each  
18 side and powder/solid portions are selectively arranged,  
19 predicted by design and computer simulation<sup>37</sup>). The structure is  
20 expected to exhibit a triaxial anisotropic Young's modulus for  
21 each axis. Triaxial anisotropy can be achieved in real molded  
22 objects, with the expression of isotropy/anisotropy by such  
23 internal structure control determined by the number of supports  
24 parallel to the load as well as point/line/surface contact<sup>37</sup>).

25 Adding such an internal structure directly controls the

1 macroscopic mechanical properties of the structure, making it an  
2 extremely useful method of utilizing the characteristics of metal  
3 AM.

4

#### 5 **4.2. Control of material properties**

6 Metal AM excels at free shape control as outlined in Section  
7 4.1, and the unique directionality of the heat flux in the molten  
8 pool, cyclic melting/solidification, and thermal profile enable  
9 controlling material properties such as microstructure and atomic  
10 arrangement. A notable feature unique to metal AM is texture  
11 control, including single crystallization<sup>6-18</sup>). Direction control  
12 and single crystallization achieve anisotropic mechanical  
13 properties, such as Young's modulus, and enable the selective  
14 control of physical property values according to the application,  
15 even for the same material. Conventional monocrystal production  
16 methods are lengthy and cannot obtain sufficient shapes and sizes,  
17 thus limiting their commercialization. However, metal AM has  
18 yielded increased expectations for realizing large monocrystal  
19 products.

20 Single crystallization enables the creation of bone implants  
21 capable of suppressing stress shielding<sup>2,4</sup>). A  $\beta$ -type Ti alloy with  
22 a bcc structure exhibits a relatively low Young's modulus, even  
23 in a polycrystalline state, but single crystallization results in an  
24 anisotropic Young's modulus that depends on crystal orientation.  
25 As shown in Fig. 6, Young's modulus represents the minimum



1 value along  $\langle 001 \rangle$  direction<sup>38,39</sup>). The elastic stiffness constant  
2 ( $c'$ ) depends on valence electron density ( $e/a$ ) (Fig. 6(a)), so  
3 Young's modulus  $E_{001}$  and its anisotropic  $E_{111}/E_{001}$  depend on  $e/a$ ;  
4 as  $e/a$  decreases and approaches the value of 4,  $E_{111}/E_{001}$   
5 increases and  $E_{001}$  decreases (Fig. 6(b)).

6 The Ti-15Mo-5Zr-3Al (mass%) alloy, with a small  $e/a$  of 4.10  
7 and approved by the ISO (ISO 5832-14)<sup>40</sup>), exhibits a low Young's  
8 modulus of approximately 85 GPa in a polycrystalline state.  
9 Furthermore, single crystallization results in  $E_{100}$  decreasing to  
10 44.4 GPa<sup>37</sup>), which is low compared to Young's modulus of  
11 cortical bone (~30 GPa); stress shielding is expected to be  
12 suppressed when  $\langle 001 \rangle$  is placed parallel to the long axis of the  
13 long bone<sup>2</sup>).

14 Applying the laser beam method and metal AM to this alloy  
15 enables selective shaping of the crystal growth orientation using  
16 scan strategy control. As shown in Fig. 7, the crystallographic  
17 orientation in the modeled object depends on the scan strategies  
18 X and XY; in either case,  $\langle 001 \rangle$  can be preferentially oriented  
19 with a low Young's modulus in a specific direction in the modeled  
20 object<sup>6</sup>). Crystallographic orientation control is determined by  
21 the movement direction of the solid-liquid interface during  
22 solidification into the molten pool, stability of the smooth  
23 surface, and the priority of the crystal growth orientation. In this  
24 case, the  $\langle 001 \rangle$  preferred crystal orientation exhibited a low  
25 Young's modulus of approximately 70 GPa, while Young's

1 modulus of the  $\langle 011 \rangle$  preferred crystal orientation was  
2 approximately 100 GPa; metal AM enabled the creation of objects  
3 with material anisotropy. Further increasing the integration of  
4 crystallographic orientation and optimal composition control that  
5 considers the evaporation of light elements is expected to result  
6 in Young's modulus approaching the theoretical value of single  
7 crystal and achieving a value similar to that of bone<sup>6)</sup>.

## 8 9 **5. Unique Material Structure Formation and High-Order** 10 **Functionality Using Metal Additive Manufacturing**

11 As outlined in Section 4.2, metal AM can be used to vary the  
12 crystallographic orientation from site to site depending on the  
13 scanning strategy<sup>6)</sup>. Therefore, unlike other processes, the  
14 material properties of each part of a product can be changed.  
15 Furthermore, controlling the shape of the molten pool and  
16 aligning the two crystal orientations enables forming a unique  
17 material structure, such as a layered structure with a fine  
18 periodicity of 100  $\mu\text{m}$ . For example, Fig. 8 shows the atomic  
19 arrangement and mechanical properties of the SUS316L  
20 austenitic stainless-steel alloy and the anodic polarization curve  
21 in a 0.9 mass% aqueous NaCl solution<sup>11)</sup>. The modeled object  
22 forms a layered structure comprising two layers (main layer and  
23 sublayer) with different crystal orientations. The unique layered  
24 structure of SUS316L leads to a decrease in strain  
25 transmissibility at the interface because the stress transfer

1 coefficient at the interface decreases from the value of 1, leading  
2 to increased strength<sup>11</sup>). Furthermore, the quenching effect of  
3 laser beam metal AM imparts a corrosion resistance that  
4 significantly exceeds that of conventional materials by  
5 eliminating MnS-based precipitates and other causes of pitting  
6 corrosion, as shown in Fig. 8(c). These observations are also  
7 currently being confirmed in various other stainless-steel grades.

8 In metal AM, attention has recently focused on a new class of  
9 materials: high-entropy alloys (HEAs) comprising five or more  
10 elements. Strong solid-solution hardening is expected due to the  
11 high-entropy effect, but conventional melting/solidification  
12 methods exhibit strong segregation and do not exhibit ideal  
13 solid-solution strengthening. AM can achieve rapid cooling of  
14 approximately  $\sim 10^7$  K/s when using a laser as a heat source; thus,  
15 the segregation prevention effect is recognized, as shown in Fig.  
16 9. As a result, the expression of functionalities unique to metal  
17 AM based on microstructure control is ever-expanding, such as  
18 imparting high strength and shape by an ideal forced solid  
19 solution<sup>13</sup>).

20

## 21 **6. Conclusion**

22 Metal AM technology can control complex external shapes and  
23 their internal structure, microstructure, and atomic arrangement  
24 as well as design functions determined by these aspects. Metal  
25 AM can also control the microstructure and atomic arrangement

1 of materials with customized material properties for each part,  
2 which is unique to metal AM. The simultaneous control of  
3 complex shapes and material properties according to each part  
4 can be considered a new high-value-added manufacturing process  
5 only achievable in the DX age. Additionally, metal AM  
6 technologies are expected to be widely used in the future for  
7 modeling bulk materials as well as a surface treatment  
8 technology involving atomic arrangement and microstructure  
9 control; thus, it has the potential to develop into a new surface  
10 control technology deeply related to thermal spraying  
11 technologies. Hence, custom-shaped objects can be created based  
12 on new ideas that control functions according to the bulk and  
13 surface parts of products that have been thus far designed based  
14 on their shape. Metal AM technologies are expected to further  
15 develop and expand into new markets, incorporating new product  
16 designs and development concepts unique to metal AM, including  
17 its concepts of isotropy and anisotropy.

18

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7    (JP25220912, JP18H052540).

## 9    **References**

- 10    1)    Osaka University Anisotropic Design & Additive  
11        Manufacturing Research Center (Osaka University Metal AM  
12        Center) website: <http://www.mat.eng.osaka-u.ac.jp/sipk/am/>
- 13    2)    T. Nakano and T. Ishimoto: *Bull. Iron Steel Inst. Jpn.* **24**  
14        (2019) 21-30.
- 15    3)    T. Nakano: *Mech. Eng.* **67** (2019) 21-27.
- 16    4)    T. Nakano: *J. Jpn. Weld. Soc.* **89** (2020) 27-37.
- 17    5)    Strategic Innovation Promotion (SIP) / “Materials Integration”  
18        for Revolutionary Design System of Structural Materials  
19        website: <https://www.jst.go.jp/sip/p05/index.html>
- 20    6)    T. Ishimoto, K. Hagihara, K. Hisamoto, S.-H. Sun and T.  
21        Nakano: *Scr. Mater.* **132** (2017) 34-38.
- 22    7)    M. Todai, T. Nakano, T. Liu, H. Y. Yasuda, K. Hagihara, K.  
23        Cho, M. Ueda and M. Takayama: *Addit. Manuf.* **13C** (2017) 61-  
24        70.
- 25    8)    K. Hagihara, T. Nakano, M. Suzuki, T. Ishimoto, S. Yalatu and

- 1 S.-H. Sun: *J. Alloy. Compd.* **6965** (2017) 67-72.
- 2 9) S.-H. Sun, K. Hagihara and T. Nakano: *Mater. Design.* **140**  
3 (2017) 307-316.
- 4 10) H. Amano, Y. Yamaguchi, T. Sasaki, T. Sato, T. Ishimoto and  
5 T. Nakano: *J. Smart Proc.* **8** (2019) 102-105.
- 6 11) S.-H. Sun, T. Ishimoto, K. Hagihara, Y. Tsutsumi, T. Hanawa  
7 and T. Nakano: *Scr. Mater.* **159** (2019) 89-93.
- 8 12) O. Gokcekaya, N. Hayashi, T. Ishimoto, K. Ueda, T.  
9 Narushima and T. Nakano: *Addit. Manuf.* **36** (2020) 101624.
- 10 13) T. Ishimoto, R. Ozasa, K. Nakano, M. Weinmann, C. Schnitter,  
11 M. Stenzel, A. Matsugaki, T. Nagase, T. Matsuzaka, M. Todai,  
12 H.S. Kim and T. Nakano: *Scr. Mater.* **194** (2021) 113658.
- 13 14) O. Gokcekaya, T. Ishimoto, S. Hibino, J. Yasutomi, T.  
14 Narushima and T. Nakano: *Acta Mater.* **212** (2021) 116876.
- 15 15) A. Takase, T. Ishimoto, R. Suganuma and T. Nakano: *Scr.*  
16 *Mater.* **201** (2021) 113953.
- 17 16) T. Ishimoto, K. Hagihara, K. Hisamoto and T. Nakano: *Addit.*  
18 *Manuf.* **43** (2021) 102004.
- 19 17) Y. Tsutsumi, T. Ishimoto, T. Oishi, T. Manaka, P. Chen, M.  
20 Ashida, K. Doi, H. Katayama, T. Hanawa and T. Nakano: *Addit.*  
21 *manuf.* **45** (2021) 102066.
- 22 18) K. Cho, H. Kawabata, T. Hayashi, H.Y. Yasuda, H. Nakashima,  
23 M. Takeyama and T. Nakano: *Add. Manuf.* **46** (2021) 102091.
- 24 19) R. Lakes: *Nature.* **361** (1993) 511-515.
- 25 20) T. Nakano, K. Kaibara, Y. Tabata, N. Nagata, S. Enomoto, E.

- 1 Marukawa and Y. Umakoshi: *Bone*. **31** (2002) 479-487.
- 2 21) Y. Shinno, T. Ishimoto, M. Saito, R. Uemura, M. Arino, K.  
3 Marumo, T. Nakano and M. Hayashi: *Sci. Rep.* **6** (2016)  
4 srep19849.
- 5 22) W.J. Landis: *Bone*. **16** (1995) 533-544.
- 6 23) T. Nakano, K. Kaibara, T. Ishimoto, Y. Tabata and Y.  
7 Umakoshi: *Bone*. **51** (2012) 741-747.
- 8 24) T. Ishimoto, T. Nakano. Y. Umakoshi, M. Yamamoto and Y.  
9 Tabata: *J. Bone Miner. Res.* **28** (2013) 1170-1179.
- 10 25) J.-W. Lee, A. Kobayashi and T. Nakano: *J. Bone Miner. Metab.*  
11 **35** (2017) 308-314.
- 12 26) A. Sekita, A. Matsugaki and T. Nakano: *Bone*. **97** (2017), 83-  
13 93.
- 14 27) T. Moriishi, R. Ozasa, T. Ishimoto, T. Nakano, T. Hasegawa,  
15 T. Miyazaki, W. Liu, R. Fukuyama, Y. Wang, H. Komori, X.  
16 Qin, N. Amizuka and T. Komori: *PLoS Getet.* **16** (2020)  
17 e1008586.
- 18 28) R. Ozasa, T. Ishimoto, S. Miyabe, J. Hashimoto, M. Hirao, H.  
19 Yoshikawa, and T. Nakano: *Calcif. Tissue Int.* **104** (2019) 449-  
20 460.
- 21 29) T. Nakano and T. Ishimoto: *Jpn. J. Appl. Phys.* **10** (2018) 759-  
22 763.
- 23 30) T. Kakeshita, T. Tanaka, T. Nakano, H. Araki, M. Furutera,  
24 K. Yamaguchi, K. Nishida and M. Teranishi: *Materia Jpn.* **25**  
25 (2015) 419-521.

- 1 31) Technology Research Association for Future Additive  
2 Manufacturing, website: <https://www.trafam.or.jp/index.html>
- 3 32) M. Demura: *J. Smart Proc.* **10** (2021) 78-84.
- 4 33) K. Cho, R. Kobayashi, J.-Y. Oh, H. Y. Yasuda, M. Todai, T.  
5 Nakano, A. Ikeda, M. Ueda and M. Takeyama: *Intermetallics.*  
6 **95** (2018) 1-10.
- 7 34) N. Raghavan, R. Dehoff, S. Pannala, S. Simunovic, M. Kirk,  
8 J. Turner, N. Carlson and S.S. Babu: *Acta Mater.* **112** (2016)  
9 303-314.
- 10 35) T. Nakano: *J. Jpn. Inst. Light Met.* **67** (2017) 470-480.
- 11 36) T. Nakano and T. Ishimoto: *Materia Jpn.* **58** (2019) 181-187.
- 12 37) T. Nakano, H. Fukuda and H. Takahashi: **879** (2016) 1361-  
13 1364.
- 14 38) S.-H. Lee, M. Todai, M. Tane, K. Hagihara, H. Nakajima and  
15 T. Nakano: *J. Mech. Behav. Biomed. Mater.* **14** (2012) 48-54.
- 16 39) M. Tane, S. Akita, T. Nakano, K. Hagihara, Y. Umakoshi, M.  
17 Niinomi and H. Nakajima: *Acta Mater.* **56** (2008) 2856-2863.
- 18 40) ISO 5832-14:2007, Implants for surgery - Metallic materials  
19 -Part 14: Wrought titanium 15-molybdenum 5-zirconium 3-  
20 aluminium alloy, (2007).
- 21



1 **List of Captions**

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3 Additive Manufacturing Research Center (Osaka University AM  
4 Center).

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6 Fig. 2. Conceptual diagram of isotropy and anisotropy. The Osaka  
7 University AM Center considers anisotropy as its design concept  
8 and aims to “construct anisotropic materials science”.

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11 cortical bone. The *c*-axes of collagen and apatite crystallites are  
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13 the bone location. Long and vertebral bones show uniaxial  
14 orientation, the skull shows two-dimensional orientation, and the  
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8

Advance View

1 **Figures**

2

**Anisotropic Design and Additive Manufacturing Research Center, Osaka University  
(Osaka university AM center)**

Established in December 2014.

**Purpose**

- Conducting research and development of innovative technologies such as additive manufacturing (AM) that enable the design and manufacture of valuable products.
- Establishing a base that connects different players involved in manufacturing.

**Main equipment**

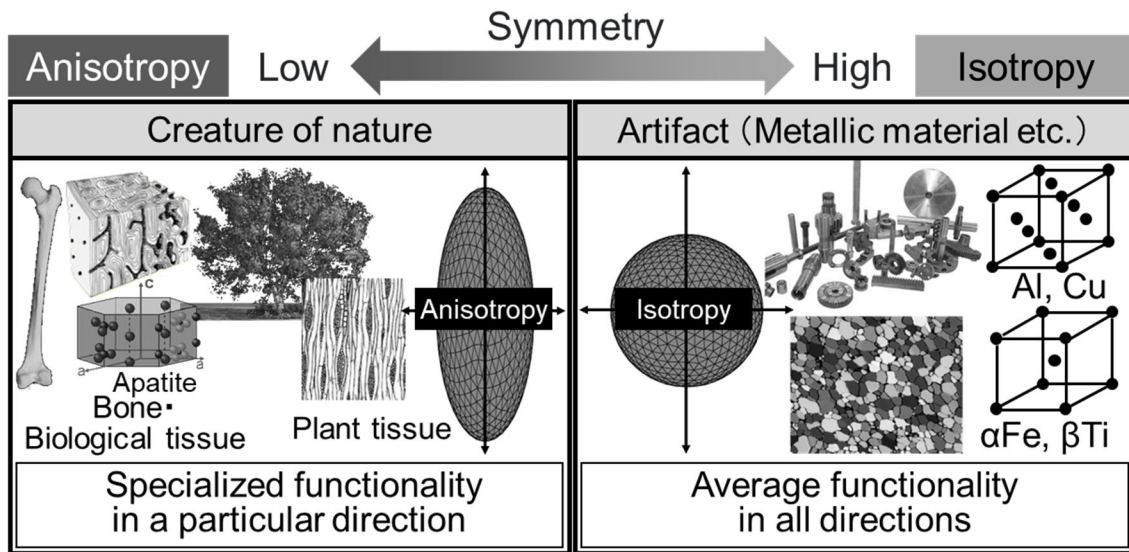
- Metal AM equipment (2 units each of electron beam and Laser beam method)
- In process monitoring system
- Process prediction by Simulation
- Powder characterization equipment etc.



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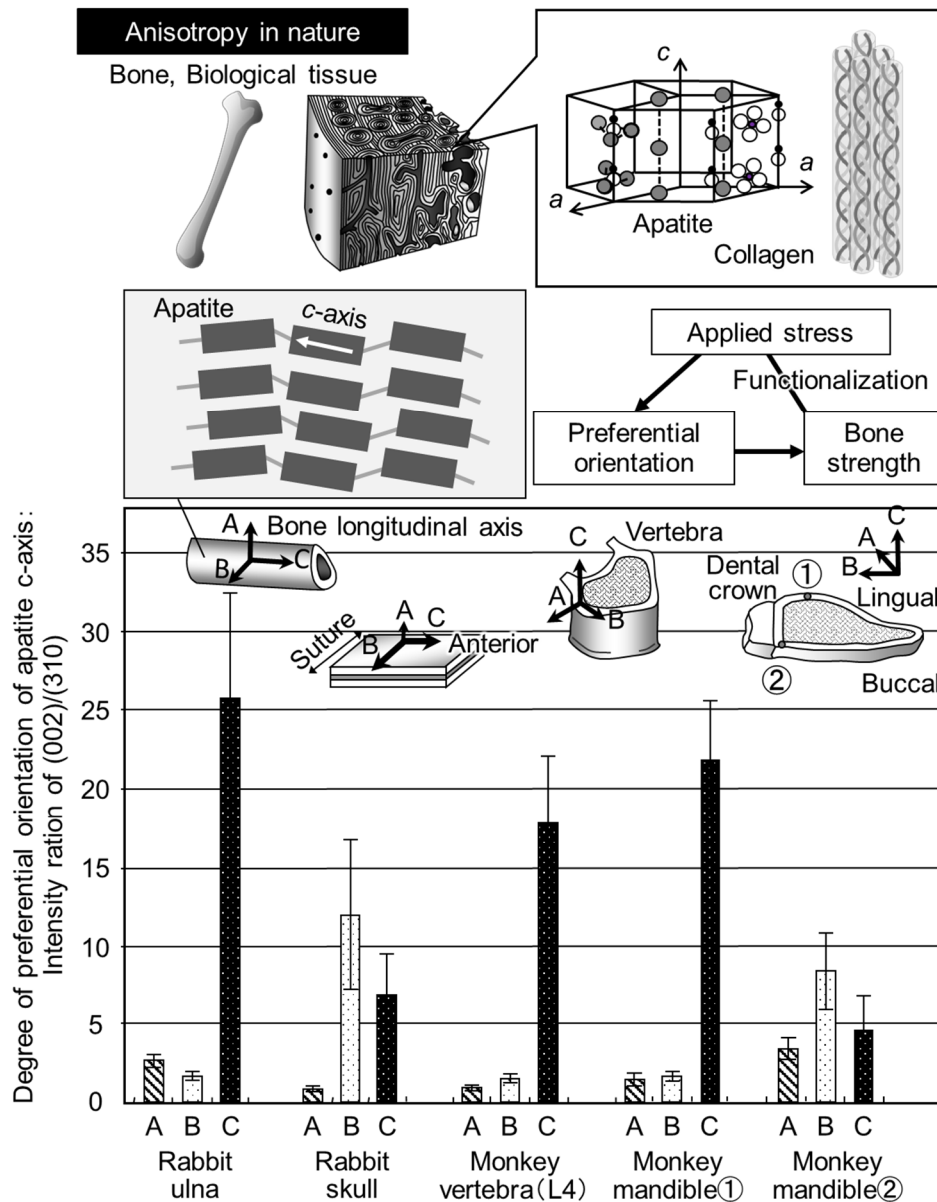
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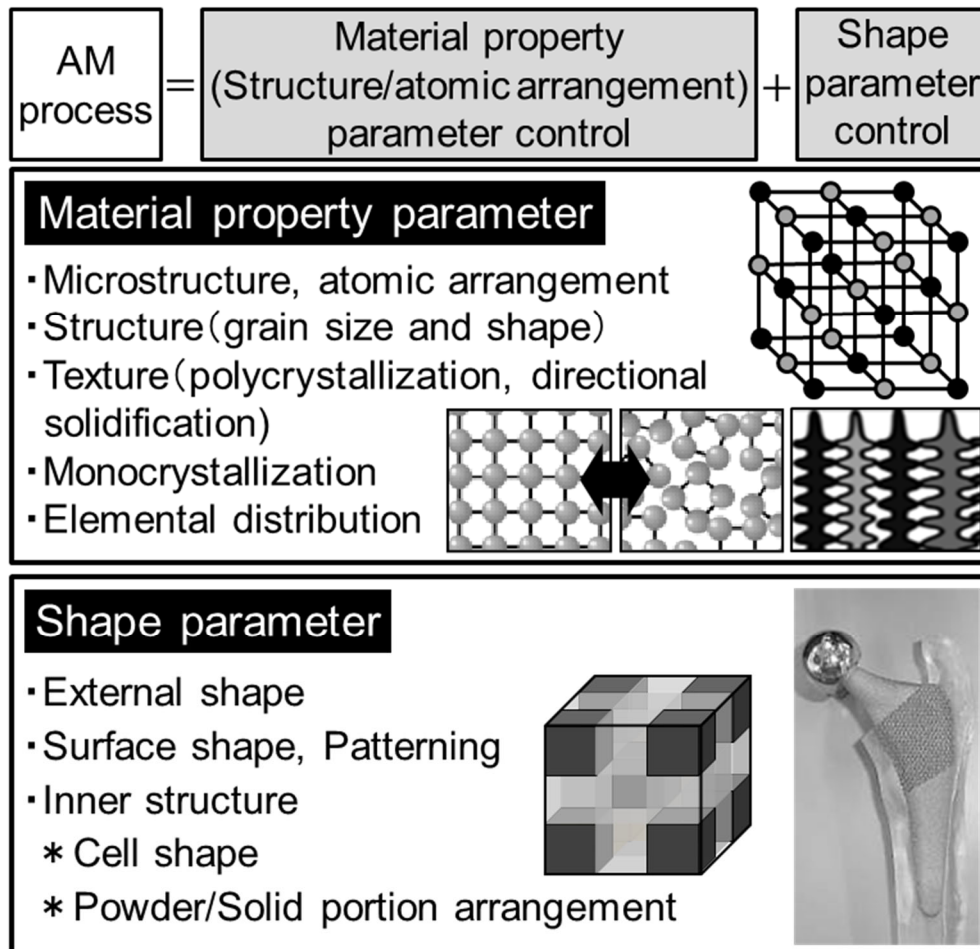
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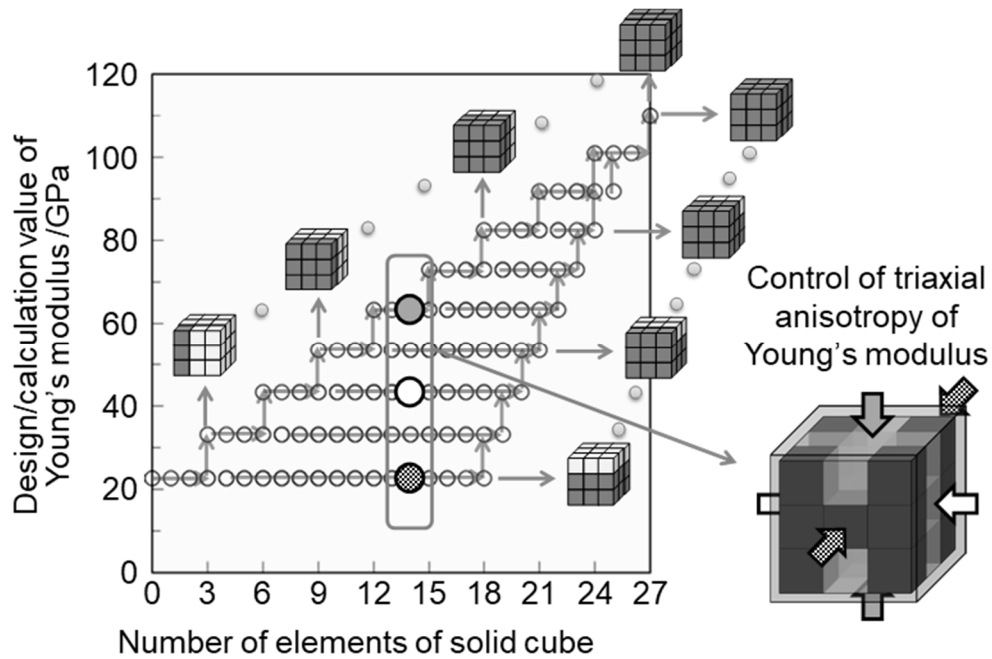
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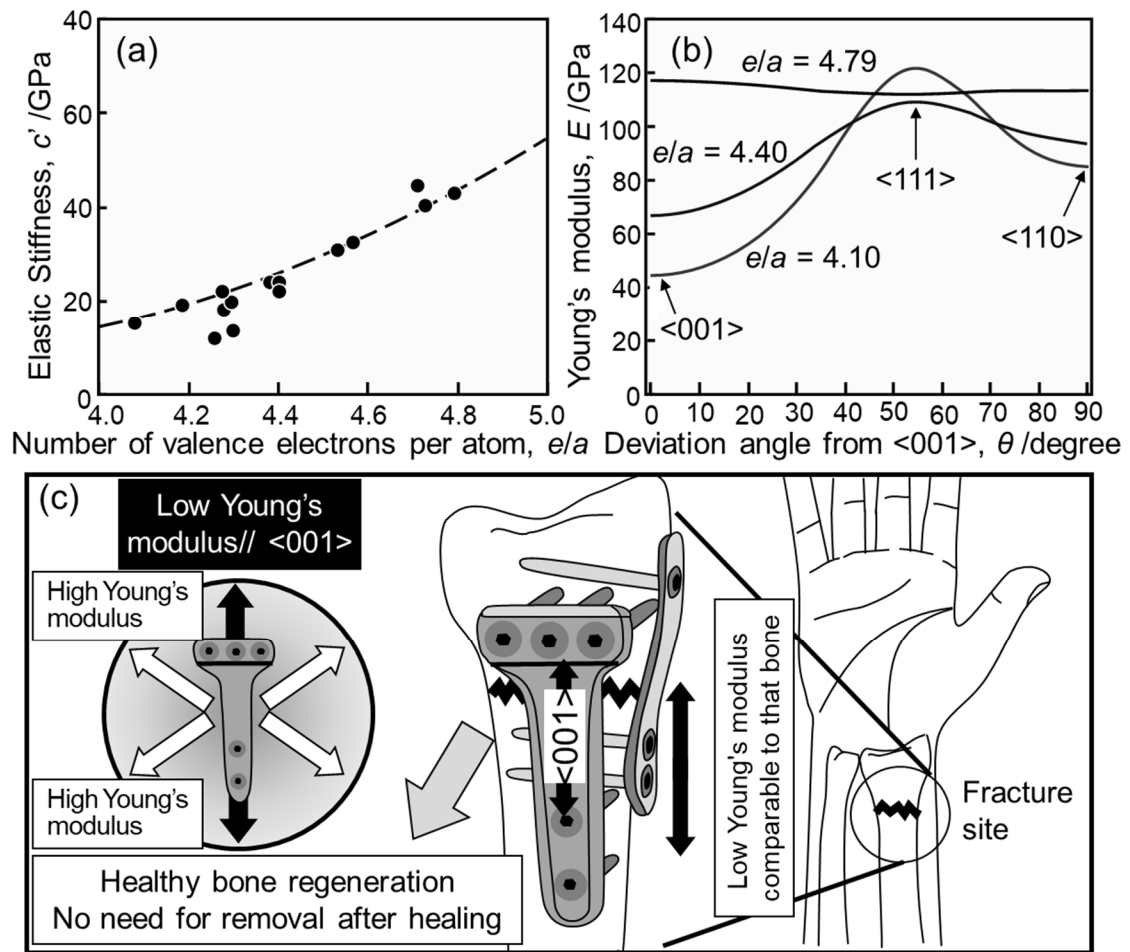


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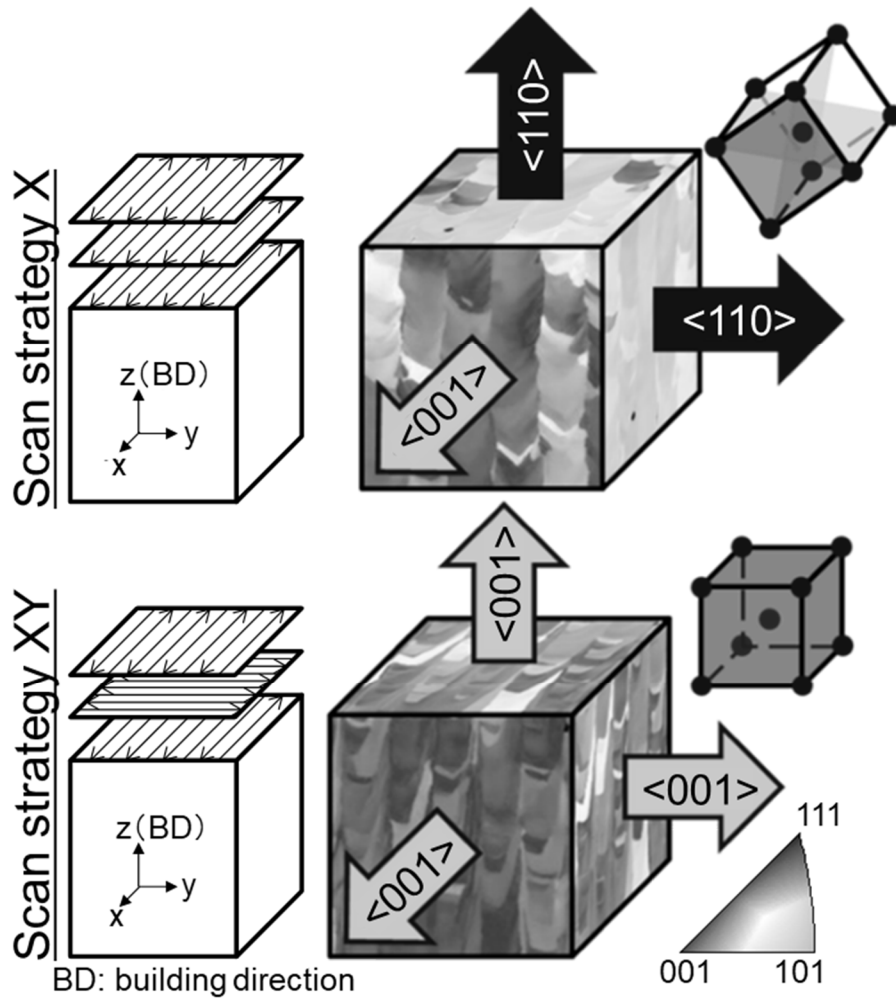
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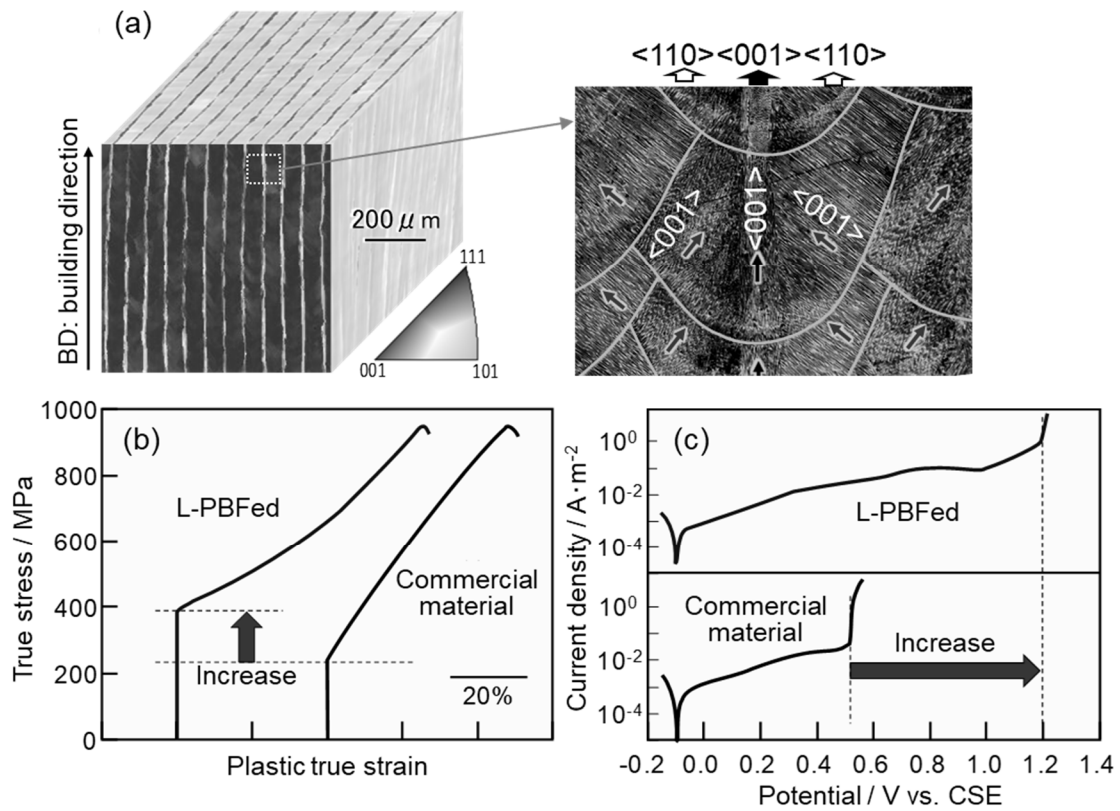
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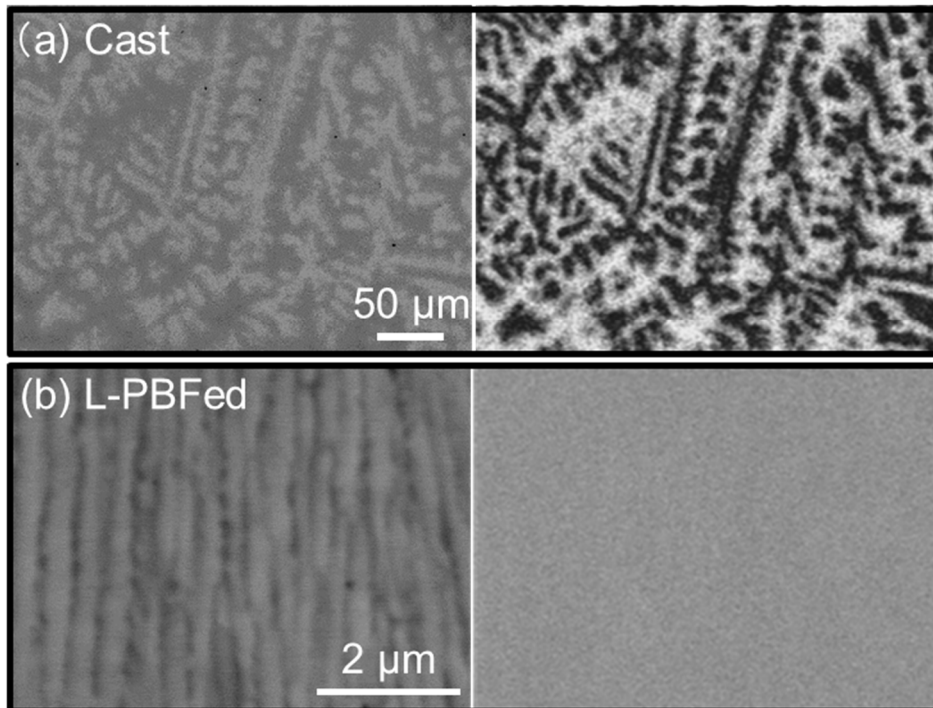
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## Backscatter electron image Elemental distribution



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